

CIV-E4010 Finite Element Methods in Civil Engineering Examination, April 18, 2023 / Niiranen

This examination consists of 3 problems rated by the standard scale 1...6. Neither course material nor calculators are allowed – pen(cil) and paper only.

Problem 1

Let us consider the finite element method in the context of *structural mechanics* and the *theory of elasticity*.

- (i) Briefly sketch the *linear Lagrange*-type *Timoshenko beam* finite element: (1) identify the number of nodes in one element; (2) list the degrees of freedom present at each node; (3) determine the size of both the local stiffness matrix and the force vector of the element?
- (ii) Briefly sketch the *quadratic Lagrange*-type *Timoshenko beam* finite element: (1) identify the number of nodes in one element; (2) list the degrees of freedom present at each node; (3) determine the size of both the local stiffness matrix and the force vector of the element?
- (iii) Briefly explain, preferably with a few formulae, what is meant by *numerical locking* in the context of *Timoshenko beam* elements.

Problem 2

Let us consider the finite element method in the context of *structural mechanics* and the *theory of elasticity*.

- (i) The governing differential equation of the *linear buckling* problem of elastic beams following the *Euler–Bernoulli beam* theory can be written in the form

$$(EIw'')''(x) + Pw''(x) = 0, 0 < x < L.$$

Write down (without deriving) the corresponding weak form by assuming that both ends of the beam are simply supported: "*Find...such that...*".

- (ii) Use one *Hermite*-type finite element for finding an approximate solution to the problem of item (i): (1) form the required finite element system equation; (2) form the characteristic equation of the problem.

For constructing the finite element equation system for the problem, there is no need to start from the basis functions: the *stiffness matrix* and

geometric stiffness matrix of the element are given, respectively, as

$$\mathbf{K} = \frac{EI}{L^3} \begin{pmatrix} 12 & 6L & -12 & 6L \\ & 4L^2 & -6L & 2L^2 \\ & & 12 & -6L \\ & & & 4L^2 \end{pmatrix}$$

$$\mathbf{K}_g = \frac{1}{30L} \begin{pmatrix} 36 & 3L & -36 & 3L \\ & 4L^2 & -3L & -L^2 \\ & & 36 & -3L \\ & & & 4L^2 \end{pmatrix}.$$

Problem 3

Let us consider the finite element method in the context of *structural mechanics* and the *theory of elasticity*.

- (i) When solving the basic problems of *linear statics*, the resulting algebraic equation system can be written in the form $\mathbf{K}\mathbf{d} = \mathbf{f}$.
- (1) Write down the equation system for the corresponding problem of *linear dynamics*. (2) Briefly explain the essential content of the system and its physical background. (3) Briefly explain the main differences in solving the equation systems of these two problem types (*linear statics* and *linear dynamics*).
- (ii) For a conforming finite element method of the *Kirchhoff plate* problem, (with certain additional assumptions) the basic mathematical finite element error estimate is of the form

$$\|w - w_h\|_2 \leq Ch^{k-1}|w|_{k+1}.$$

Define and name the quantities, variables, indices and other notation appearing in the inequality, and shortly describe the information this estimate provides.

- (iii) For isotropic materials, the moment vector of the *Kirchhoff plate* problem can be written as

$$\mathbf{M}(\nabla w) = \mathbf{D}\boldsymbol{\kappa}(\nabla w)$$

$$\mathbf{D} = D \begin{pmatrix} 1 & \nu & 0 \\ \nu & 1 & 0 \\ 0 & 0 & (1-\nu)/2 \end{pmatrix}, \quad D = \frac{Et^3}{12(1-\nu^2)}$$

$$\boldsymbol{\kappa}(\nabla w) = \begin{pmatrix} -\partial^2 w / \partial x^2 \\ -\partial^2 w / \partial y^2 \\ -2\partial^2 w / \partial x \partial y \end{pmatrix}.$$

By utilizing the error estimate given in item (ii), write down an error estimate for the finite element approximation of the bending moment.