a State space presentation is a motheratical motel of a physical system as a set of input, output and state variables related by differential equations. The variables are expressed as vectors and the differential and algebraic equations are written in matrix form S-17.162 Advanced course in Electromechanics =5-17,3020 Examination 28.04.2005, 12 –15 o'clock, Lecture room I 256. 1. Explain briefly a) the basic machine with four windings, b) small-signal analysis of electrical machines,

- c) state-space presentation of a system of differential equations,
- d) what does a space-vector of a three-phase stator current mean,
- e) the four basic assumptions of space-vector theory. If the dentity in the area gop of an electrical machine is zinusoidally distributed Dylagnetisation culve is a straight line 3) Thou losses can be neglected 4) Resistances and inductances are interendent from frequency
- a) An electrical machine has symmetric three-phase windings both in the stator and rotor.

a) An electrical machine has symmetric three-phase windings both in the stator and rotor. Starting from equation
$$u = Ri + \frac{d\psi}{dt}, \quad v_r = k_r i_r + \frac{d\psi}{dt}, \quad v_r = v_r^2 e^{ivk}, \quad \psi_r = v_r^2 e^{ivk}, \quad \psi_r = v_r^2 e^{ivk} = k_r i_r^2 e^{ivk}, \quad \psi_r = k_r^2 e^{ivk} + k_r^2 e^{ivk}$$

derive the voltage equations of the stator and rotor windings in the stator frame of reference when the flux linkages  $\psi$  are expressed as functions of the currents.

b) Separate the vector equations into real and imaginary parts, and present the system of  $\omega_h = \frac{dv^2 l}{dx}$ equations in the matrix form of the two-axis theory.

a) Show that the instantaneous power can be calculated in terms of vector quantities as

$$P = \frac{3}{2} \operatorname{Re} \left\{ \underbrace{ui^*} \right\}. \quad \int_{3}^{2} \left\{ \underbrace{v_{Sa} + a \underbrace{w_{Sb} + a^2 v_{Sc}}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a \underbrace{w_{Sb} + a^2 v_{Sc}}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a \underbrace{w_{Sb} + a^2 v_{Sc}}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a \underbrace{w_{Sb} + a^2 v_{Sc}}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a \underbrace{w_{Sb} + a^2 v_{Sc}}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a \underbrace{w_{Sb} + a^2 v_{Sc}}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a \underbrace{w_{Sb} + a^2 v_{Sc}}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a \underbrace{w_{Sb} + a^2 v_{Sc}}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a \underbrace{w_{Sb} + a^2 v_{Sc}}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a \underbrace{w_{Sb} + a^2 v_{Sc}}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa} + a^2 v_{Sc}}_{3} \right\} \left\{ \underbrace{v_{Sa}$$

- b) Derive also the instantaneous torque expressed in terms of vector quantities. = \frac{2}{3} [\omega\_{\infty} \frac{1}{2} \omega\_{\infty} \f
- = Usaisa+Useisp+Uscisc konh a) Transform the space-vector voltage and flux equations of a cage induction motor to the  $\log \frac{1}{2} = \log \frac{1}{2}$ equations of the small-signal theory.
- b) The stator voltage of the machine running at the rated load changes slightly. Derive the equations for the resulting changes in the stator and rotor currents.

Instruction: Assume that the speed remains constant during this transient, i.e. the change in the speed can be neglected.

A permanent magnet synchronous motor is driving a gas turbine at its rated power ( $U = U_n$ ,  $I = I_{\rm n}$ ,  $\cos \phi = 1$ ,  $T = T_{\rm n}$ ,  $\Omega = \omega_{\rm n}/p$ ) when it is suddenly disconnected from the voltage supply. Derive an equation giving the stator voltage after the disconnection. The machine has no damper winding. The parameters of the stator winding are  $R_s$ ,  $L_d = L_q$ . The torque of the turbine is proportional to the second power of the rotation speed, and the common moment of inertia of the system is J.

Instruction: After the disconnection, the permanent magnets in the rotor produce a constant flux, the amplitude of which can be calculated from the rated values. The frequency of the flux in the stator changes according to the equation of motion. All the losses of the electrical motor are assumed to be zero.